FIG. 1A

DYNAMICALLY ADJUSTABLE DIGITAL GYRATOR HAVING EXTENDED FEEDBACK

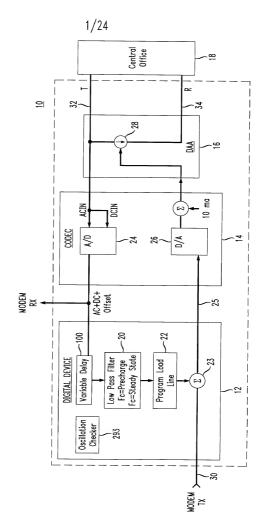


FIG. 1B

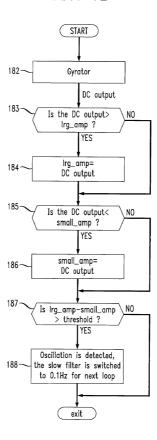
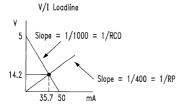
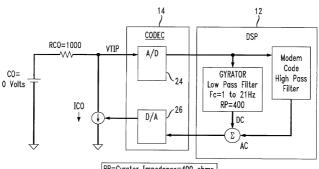


FIG. 2A



50-ICO*RCO=ICO*RP=VP ICO=14.27 mA VP=35.7 Volts Note: All results are at steady state

 $FIG.\ 2B$ DYNAMICALLY ADJUSTABLE DIGITAL GYRATOR EXAMPLE



RP=Gyrator Impedance=400 ohms RCO=Central Office Resistance

FIG. 3A

CODEC and Telephone System Stability Block Diagram

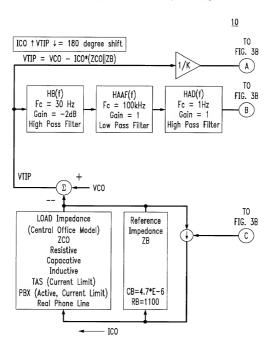


FIG. 3B

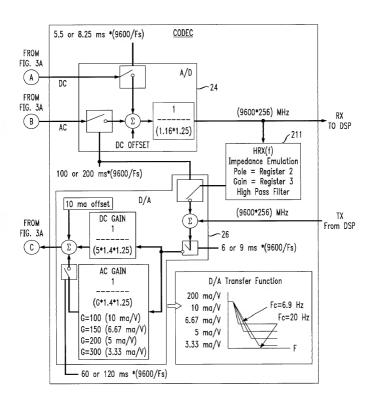


FIG. 4

Simplified D/A Path

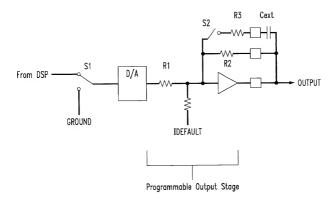
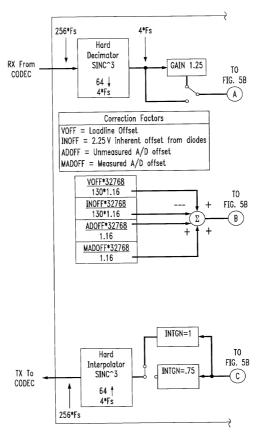


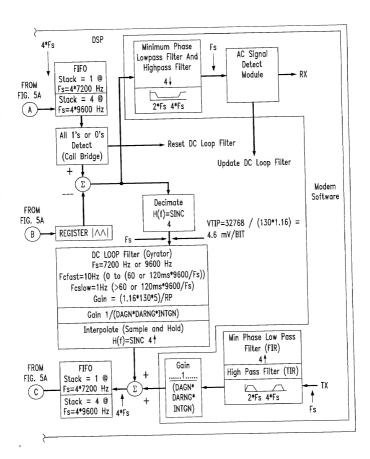
FIG. 5A

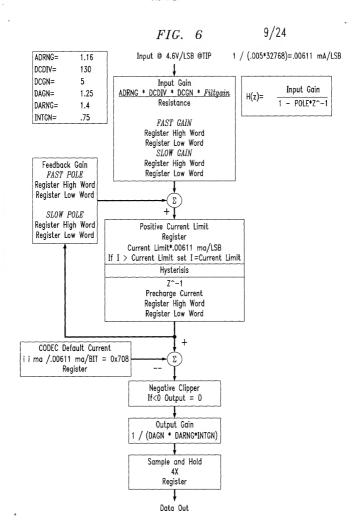




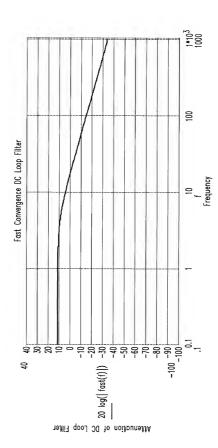
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FIG. 5B





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FI

FIG.~7B 10 Hz Fast DC Loop Filter Gain and Phase

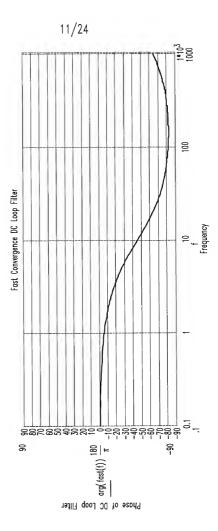
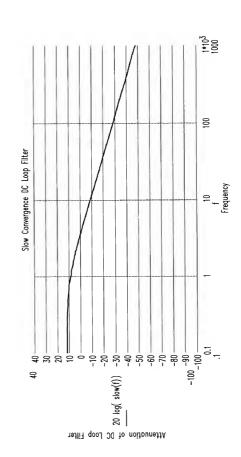


FIG. 8A

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9 Slow Convergence DC Loop Filter 1 Hz Slow DC Loop Filter Gain and Phase 9 $arg(slow(f)) \frac{180}{\pi}$

Phase of DC Loop Filter

FIG. 9

First Order Filter Topology

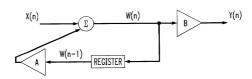
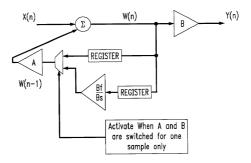
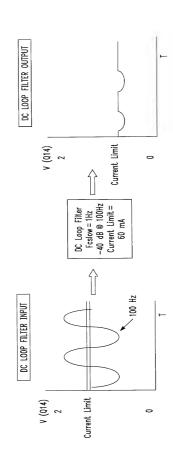


FIG. 10

Final Low Pass Topology with glitch removed



DC Loop Filter Without Hysterysis FIG. 11A



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DC LOOP FILTER OUTPUT Lower Hysterysis Limit v (014) 2 Current Limit 0 DC Loop Filter
Fcslow = 1Hz
-40 dB @ 100Hz
Current Limit = 60 mA 100 Hz DC LOOP FILTER INPUT v (q14) 2 Current Limit 0

FIG. 11B

DC Loop Filter With Hysterysis

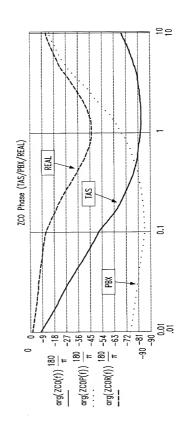
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우은 ZCO Magnitude (TAS/PBX/REAL) Hz TAS 5 æ 0.0 Ohms 200000 2*105 | 16*105 | 16*105 | 125*105 | 2000(f) | 1.2*105 | 2000(f) | 8*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 4*104 | 9

FIG. 12A

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FIG.~~12B TAS, PBX and Real Phone Line V/1 Loadlines



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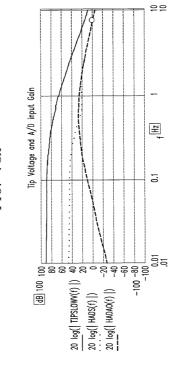
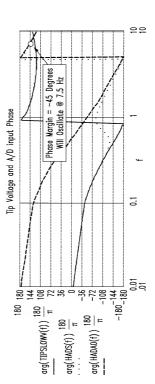


FIG. 13A

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 $FIG. \quad \textit{1} \ 3B$ TAS Termination with Lowpass Filter Cutoff = 1 Hz



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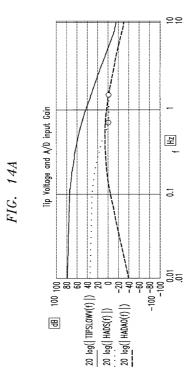
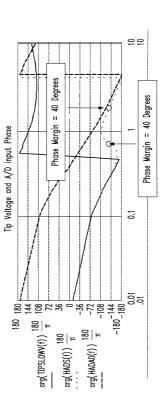


FIG. 14B

TAS Termination with Lowpass Filter Cutoff = .1 Hz



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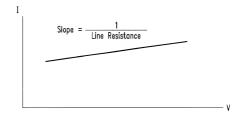


FIG. 16

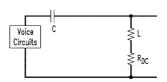


FIG. 17

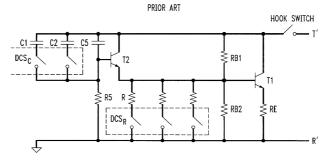
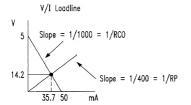


FIG. 18A



50-ICO*RCO=ICO*RP=VTIP ICO=14.27 mA VP=35.7 Volts Note: All results are at steady state

FIG. 18B

Basic External Gyrator Example

